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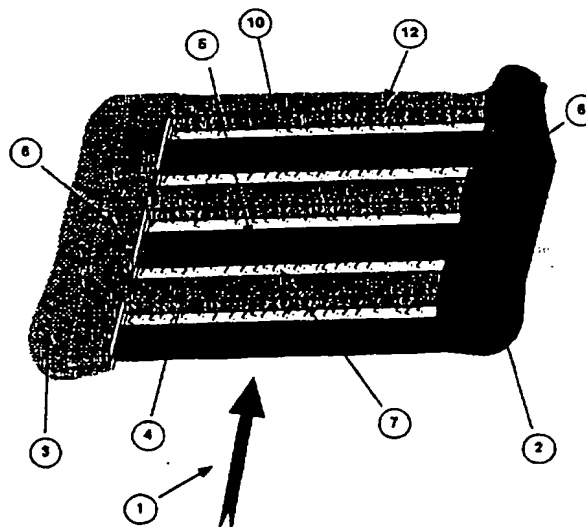
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(54) Title: IMPEDIMETRIC DETECTION SYSTEM AND METHOD OF PRODUCTION THEREOF

(57) Abstract

A sensor for identifying molecular structures within a sample solution is disclosed. The sensor comprises an insulating layer with a plurality of interspaced channels therein having essentially the same direction. Said channels have a bottom and at least two opposite side-walls along said direction. The channels furthermore have submicron dimensions. A metal coating is applied on one of said two opposite side-walls of essentially each channel and on top of the dielectric layer inbetween said channels thereby forming an impedimetric device with said sample solution within and between adjacent channels. Probes for specifically binding to said molecular structures can be applied, said probes being applied to either the insulating part of the channels (said bottom and the other side-wall of said channels), or to the surface of the electrodes or both, the insulating part of the channels and the surface of the electrodes. Furthermore, means are provided for applying a voltage on the metal coatings; and means for measuring the impedance inbetween the electrodes. Furthermore, a method of fabricating a sensor for identifying molecular structures within a sample solution is disclosed. This method comprises the steps of forming a plurality of interspaced channels in an insulating layer, said channels having essentially the same direction, said channels having a bottom and at least two opposite side-walls along said direction; depositing a metal layer on said insulating layer while aligning said insulating layer with respect to the metal deposition source such that the bottom of said canals and the side-walls of said canals along the deposition direction are shadowed and not covered by metal to thereby form an impedimetric device with said sample solution within and between adjacent channels; and applying probes for binding to said molecular structures, said probes being applied to either the insulating part of the channels (said bottom and the other side-wall of said channels), or to the surface of the electrodes or both, the insulating part of the channels and the surface of the electrodes, facing the deposition direction.



This method comprises the steps of forming a plurality of interspaced channels in an insulating layer, said channels having essentially the same direction, said channels having a bottom and at least two opposite side-walls along said direction; depositing a metal layer on said insulating layer while aligning said insulating layer with respect to the metal deposition source such that the bottom of said canals and the side-walls of said canals along the deposition direction are shadowed and not covered by metal to thereby form an impedimetric device with said sample solution within and between adjacent channels; and applying probes for binding to said molecular structures, said probes being applied to either the insulating part of the channels (said bottom and the other side-wall of said channels), or to the surface of the electrodes or both, the insulating part of the channels and the surface of the electrodes, facing the deposition direction.

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IMPEDIMETRIC DETECTION SYSTEM AND METHOD OF PRODUCTION THEREOF

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The present invention relates to an improved sensor for electronically detecting a binding reaction between molecular structures or a pair of chemical substances, such as oligonucleotides, antigens, enzymes, peptides, antibodies, DNA and RNA fragments.

The present invention further provides a new production method for this improved sensor.

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Techniques and sensors for detecting molecular structures and specific substances such as enzymes, peptides, oligonucleotides, antigens, antibodies, DNA and RNA fragments in a solution sample are known in the art. In a specific class of sensors, use is made of the principle of measuring the impedance between two electrodes. The absence or presence of DNA-molecules or antibodies or antigens between the electrodes affects the permittivity and/or the conductivity between the electrodes. Various techniques were proposed to measure the presence and/or concentration of a given analyte in a sample solution by using a binding substance element having specific affinity for the analyte. Such specific binding reactions occur e.g. between enzymes and their substrates, antibodies and antigens, between DNA-DNA, between RNA-DNA, or other molecular structures.

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Stoner et al. in "Adsorption of blood proteins on metals using capacitance techniques", *J. Phys. Chem.*, 74, Mar. 5, 1970, describe a differential capacity measurement for evaluation of protein adsorption on metallic electrodes.

Arwin et al. in U.S.Pat. No. 4,072,576, use an adsorbed polypeptide substrate and establish a capacitive method for the measurement of enzymatic activity and the immunological interaction assay.

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Giaever in U.S.Pat. No. 4,054,646, teaches an electrical method that measures the presence of antibodies in a solution, by coating a metallic substrate with an antigen. After the incubation of the electrodes with the sample solution, he measures capacitively the thickness of the molecular sheet, i.e. he distinguishes between mono- and bimolecular layer, by using a mercury drop as a

second electrode.

Newman in Patent application WO87/03095 discloses a capacitive sensor for chemical analysis and measurement. Said sensor can be used to detect a broad range of analytes including bacteria, viruses, antibodies, antigens, enzyme substrates and hormones. A thin insulating layer is coated on the surface of conductors and a substrate to form an open capacitor. A biospecific binding agent is immobilized on the surface of the insulating layer between the conductors. The dielectric constant of the biospecific binding agent is altered by binding of the analyte being detected with the biospecific binding agent. A similar sensing principle is disclosed in U.S. Pat. 5,114,674.

Battailard et al., 1988, *Anal.Chem.*, **60**, 2374-2379 and more recently, Klein et al., 1995, *Sensors and Actuators*, **B 26-27**, pp. 474-476, show that a metal-semiconductor-insulator device can be used in a similar way as a MIS (metal-insulator-semiconductor) capacitor. The device is immersed in a solution together with a second, reference electrode. By measuring the ac capacity between the metallic layer of the device and the reference electrode, when dc biasing voltages are simultaneously applied, the flat band voltage of the system is in fact measured in a similar way as in the case of a MIS capacitor. It was proven that the flat band voltage can be modulated by species adsorbed at the insulation-liquid interface. On this principle work the ISFET, ion-sensitive-field-effect-transistor and GENFET, gene-sensitive-field-effect-transistor.

U.S.Pat. 4,219,335, issued to Richard Ebersole discusses the use of immune reagents labeled with reactance tags. These tags can be detected electrically since they alter the dielectric, conductive or magnetic properties of the test surface.

Similarly, EP 0 241 771, issued to S.J.Mroczkowski, teaches the detection of metal labeled antibodies by conductometric measurements. When antigens are immobilised inbetween two electrodes, the specific interaction with a metal-labeled antibody is measured by means of resistance decrease of the interelectrode medium.

M.Malmros in U.S. Pat. 4,334,880 describes conductivity variation of a semiconductive polymeric layer inbetween two planar electrodes. The said polymer incorporates, in a way or another, certain molecules able to recognize specific analytes. The recognition process induces conductivity changes of the polymeric layer.

Further variations on this central idea of impedimetric sensing appear in the art, EP 0 543 550,

EP 0 241 771, U.S. Pat. 4,453,126, GB 2,137,361, US 3,999,122. Essentially in an impedimetric sensor, certain molecules are immobilised on the top, in between or both on the top and in between a pair of electrodes. Said molecules 'recognise' a specific analyte when exposed to a sample solution. This recognition process eventually ends up, directly or indirectly, in conductivity and/or permittivity alteration of the space in the neighbourhood of the electrodes. Finally, by measuring the impedance between the two electrodes, a measure of the recognition process can be established.

The problem associated with the so called sensors as referred to above is that to have a good resolution, the immobilised layer should be perfectly homogenous and should not contain holes, which is hard to achieve.

With the advent of the microelectronic technology, there is a continuous effort to use it in order to develop micro-sensors. Sensors realised with microelectronic technology offer advantages such as low-cost production, increased reproducibility of the production process, uniformity, accurateness of detection, and flexibility in development. Such microelectronic sensors can comprise a multitude of individual test sites with reproducible, uniform electrical properties, whereby enhancing the detection sensitivity of the sensor. The test sites can be made with dimensions of the order of the dimensions of the molecules that have to be detected. The spatial limitations are the fabrication technology resolution and the sensitivity of the device which is dictated by the state of the art in instrumentation and the density of probes. A configuration can also be realised wherein the individual test sites can each yield a different type of signal according to the particular molecule which is to be detected in said test site.

Another important characteristic of the microelectronic technology is its planarity: the microelectrodes patterned this way are essentially flat elements. This feature is not a strong point in the impedimetric devices. In a planar impedimetric structure the electric field lines expand more above the device surface and out of the region of interest in comparison to real 3-D structures. This is a major drawback especially when the region of interest is limited in space, i.e. it is an enzymatic or polymeric membrane or an adsorbed molecular layer at the surface of the structure. Any field line departing this region of interest, introduces in the impedimetric response a shunting impedance which can be considered as noise for the measurement.

Still, depending on the electrodes geometry, i.e. dimensions and interspacing, a big majority

of the total signal is enclosed in a certain region above the surface of the device as shown in figure 1. From the same figure one can deduce that miniaturisation, i.e. L decrease, is crucial in obtaining impedimetric planar structures that probe the space in the very close neighbourhood of the device. An illustration of the dimension down scaling was given by DeSilva et al.

DeSilva et al. in 1995, *Biosensors & Bioelectronics*, 10, pp. 675-682 report a new biosensing structure that combines a covalent antibody immobilization technique with a simple impedance response method. The biosensor was fabricated by covalently binding anti-SEB antibodies onto an ultra-thin, island-like, electrically continuous, Pt film deposited onto a silicon chip. They register an impedance decrease when the specific interaction with SEB takes place.

However, the reproducibility is low due to the somewhat random behavior of the fabrication process, i.e. the Pt deposition and the immobilisation procedure.

A true electrode patterning process is likely to insure a good reproducibility of the structures and to improve the control upon sensor behaviour. Devices with patterned features, said features having dimensions of hundreds of nanometers are expected to be highly sensitive to DNA fragments of 300 bases, i.e. exhibiting a total molecular length of about 180 nm. or to other large molecules like enzymes or antibodies (tens of nanometers diameter). This dimension range is usually achieved in two ways:

1. deep UV or X-ray lithography, techniques where about 100 nm features can be achieved with a fully optimised process.

2. electron-beam patterning, a tedious and very expensive technique where features of tens of nm can be obtained.

It is an aim of the present invention to provide an electrochemical sensor suitable for measuring the presence or absence of molecular structures.

It is another aim of the present invention to provide a method for fabricating as defined above.

It is yet another aim of the present invention to provide a method for detecting the presence of molecular structures in a sample.

The present invention relates to a new electrochemical sensor, based on the interference of an electrical field between electrodes with the analyte. The analyte to be tested is brought in the close

neighbourhood of the structure by means of probes.

The present invention relates more particularly to a sensor for identifying molecular structures within a sample solution is disclosed. The sensor comprises an insulating layer with a plurality of interspaced channels therein having essentially the same direction. Said channels have a bottom and at least two opposite side-walls along said direction. The channels furthermore have
5 ~~submicron~~ dimensions. A metal coating is applied on one of said two opposite side-walls of essentially each channel and on top of the insulating layer in between said channels thereby forming an impedimetric device with said sample solution within and between the channels. Optionally probes for binding to said molecular structures are already applied on said sensor. Said probes can be applied to either the insulating part of the channels (said bottom and the other side-
10 wall of said channels), or to the surface of the electrodes or to both, the insulating part of the channels and the surface of the electrodes. Furthermore means are provided for applying a voltage on the metal coatings; as well as means for measuring the impedance in between the electrodes.

The term electrochemical sensor or shortly sensor according to the present invention refers to a device which transforms a (bio)chemical information into an electrical signal.

15 The present invention overcomes the problem of sensitivity compared to prior art sensors and methods. One important feature of this novel design is the high degree of miniaturisation. This is likely to reduce the noise of the structure and subsequently to increase its sensitivity. Another remarkable feature of the proposed sensor is its tridimensional geometry. This improves the electric field penetration in the area of interest with an eventual sensitivity increase. Said sensor
20 has an interdigitated electrode structure which can be fabricated in a cheap way, even for large active areas.

The probes of the present invention are functionally defined as molecules able to react with another molecule to form a complex an/or induce a secondary reaction. It is by the way of example and not by way of limitation that probes can be enzymes, antibodies, antigens, peptides,
25 DNA fragments, RNA fragments or oligonucleotides. Preferred probes according to the present invention are described in the following patents and patent applications held by one of the present applicants: EP 0 337 896; EP 0 345 375; EP 0 657 532; EP 0 419 355; EP 0 525 095; EP 0 494 317; EP 0489968; EP 0 644 202; WO 92/10514; EP 0 499 003; WO 92/11366; WO 92/16628; WO 92/19770; WO 93/08302; WO 93/18054; EP 0 561 087; WO 93/22437; WO 94/01554; EP

0 637 342; WO 94/13795; WO 94/18325; WO 94/21818; WO 94/25601; WO 95/12666; WO 95/17429; WO 95/33851; WO 96/00298; WO 96/04309; EP 0 721 505; WO 96/13590; WO 96/13608; WO 96/17065; and PCT applications filed under number 96/03091, 96/04146; as well as EP applications filed under No. 95870136.9, 96870006.2, 96870081.5, 96870053.4, 96870122.8 or 96870131.8. The contents of these patent (applications) and any other document referred to in this text are to be considered as incorporated by reference. The probes as well as the methods for making these probes are further discussed in the above-mentioned documents. It should be clear that these probes may be purified from a living source or may be made by any method of synthesis known in the art.

The targets to be detected in the sample or analyte can be any molecule present in a sample which binds or reacts with said probes. The targets can thus also include enzymes, antibodies, antigens, peptides, DNA fragments, RNA fragments, oligonucleotides or even whole cells. Depending on the type of targets and type of application, a specific type of recognition circuitry for processing the information related to target detection may be provided with or separately from the sensor.

The sample can be any biological sample (tissue or fluid) containing target molecules to be detected taken directly or after culturing (enrichment) from a healthy or an infected human being or animal. More specifically these samples can include expectorations of any kind, blood, plasma, respiratory tract samples such as sputum, broncheolavages, skin tissue, biopsies, lymphocyte blood culture material, colonies, cerebrospinal fluid, brain tissue, urine, gastrointestinal tract, food, feed or environmental samples. Said samples may be prepared or extracted by any method known in the art.

The sample may also be any preparation as described below (such as urea) or any other industrial product.

Alternatively, the sample to be tested may contain partially or fully purified target or analyte molecules, such as for instance amplified nucleotides, which have been solubilized in a solution. These solutions can be chosen from any type of solution known in the art which is suited for establishing a binding reaction between the specific probe and its target.

In the case of nucleotide detection, the sample material will include either genomic DNA or precursor RNA or amplified versions thereof. The solution will be what is referred to as

hybridization solution. Upon hybridisation under what is referred to as "desired hybridisation characteristics according to the present invention", the probe (in this case an oligonucleotide) will only hybridize to the DNA or RNA from the specific organisms or molecules for which it was designed and not to the DNA or RNA from other organisms or molecules such as closely related organisms or variant or mutated molecules which may also be present in a particular sample. In practice, this often implies that the intensity of the hybridization signal is at least two, three, four, five or even ten times stronger with the target DNA or RNA from the organisms from which the probes were designed, as compared to non-target sequences. Often it is desirable and achievable to detect nucleotide which perfectly match the probe nucleotide (implying that hybridization conditions are used in which one mismatch is detectable).

The hybridization conditions can be monitored relying upon several parameters, such as the nature and concentration of the components of the media or solutions, and the temperatures under which the hybrids are formed and washed. When modifications are introduced, be it either in the probes or the media, the temperatures at which the nucleotide probes can be used to obtain the required specificity should be changed according to known relationships, such as those described in Hames and Higgins (eds.). Nucleic acid hybridization. A practical approach, IRL Press, Oxford, UK., 1985.

The probes may be applied to the sensor of the present invention in any manner known in the art, for instance immobilized by means of high resolution probe dispensing systems or even synthesized on the spot.

In another set-up also comprised within the scope of the present invention, the sample may be applied to the sensor and the probes may be added in solution to the active test site area of the sensor to bring about a recognition which may be detected.

It should be stressed that the ability to simultaneously generate recognition results with a number of probes is an outstanding benefit of the sensors of the present invention.

In case of detection of antibodies present in a sample, the probe will be an antigen (e.g. a peptide or a polypeptide) or an anti-idiotypic antibody known in the art. In case of detection of antigens or polypeptides or peptides possibly present in a sample, the probe will be an antibody or a derivative thereof specifically binding to certain antigens, an antisense peptide specifically binding to certain peptides or polypeptides, a receptor or chemical molecule specifically binding

to said polypeptide or peptide. The solution in which the possibly prepared or purified target material present in the sample may be dissolved, will be any solution which allows the binding between said binding molecules to occur. The conditions under which this formation may occur are well known in the art and are for instance further described in the above-mentioned patents and applications of the one of the applicants..

5 The present invention also relates to method of fabricating a sensor for identifying molecular structures within a sample substance. This method comprises the steps of forming a plurality of interspaced channels in a insulating layer, said channels having essentially the same direction, said channels having a bottom and at least two opposite side-walls along said direction; depositing a metal layer on said insulating layer while aligning said dielectric layer with respect to the metal
10 deposition source such that the bottom of said channels and the sidewalls of said canals along the deposition direction are shadowed and not covered by metal to thereby form an impedimetric device with said sample substance within and between the channels and eventually immobilising probes for binding to said molecular structures, said probes being applied to either the insulating part of the channels (said bottom and the other side-wall of said channels), or to the surface of
15 the electrodes or to both, the insulating part of the channels and the surface of the electrodes.

 The present invention represents an important tool in a wide field of applications and it is by the way of example and not by way of limitation suited for measuring specific interactions like the reaction between an enzyme and its substrate or the recognition reaction between an antibody and an antigen, between DNA-DNA, between RNA-DNA, or other molecular structures; in the study
20 of the reaction kinetics of said specific interactions; for sequencing molecules such as peptides, enzymes, nucleotides, DNA, RNA and so on; for detecting genes mutations; for epidemiology and geno- or sero typing or for instance HLA and HCV; for drug susceptibility testing like the resistance against beta-lactamase and tetracycline in Neisseria gonorrhoeae, the detection of rifampicin resistant Mycobacterium tuberculosis strains or the detection of AZT-resistance in
25 HIV; in screening and diagnosis: viral diagnosis: like in the case of HIV, HCV, HBV, herpes and relatives, CMV, HPV or HTLV; bacterial diagnosis like in the case of sexually transmitted diseases, cerebral spinal fluid analysis, detection of different mycobacterial species, evaluation of anaerobic infections, otitis, respiratory tract, gastro-intestinal tract, periodontal pathogens, pathogenic fungi; genetic diseases, like cystic fibrosis, Alzheimer, detection of mitochondrial
30 mutations, platelet antigens, drug receptors, risk factors for atherosclerosis and coronary heart

diseases, cancer, APOE, AChE, APOB, LDL and so on; in clinical analysis: like in the case of conductometric urea or creatinine quantitation.

The high sensor miniaturisation also allows the construction of integrated microdiagnostic devices capable of simultaneous detection of a multitude of parameters, i.e. multiparameter testing, and ultimately screening assays.

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ABBREVIATIONS

	BCB	Benzocyclobuteen
	LPCVD	Low Pressure Chemical Vapour Deposition
	PECVD	Plasma Enhanced Chemical Vapour Deposition
10	PMMA	polymethylmetacrylaat
	PEEK	Poly(etherether)keton
	PC	Polycarbonaat
	PVE	Polyvinylethyleen
	PEI	Polyethyleneimine
15	CMV	Cytomegalovirus
	HPV	Human papilloma virus
	HTLV	Human T-cell leukemia virus
	APOE	Apolipoprotein E
	APOB	Apolipoprotein B
20	AchE	Acetylcholinesterase
	LDL	Low density lipoprotein
	HLA	Human leukocyte antigen
	HCV	Hepatitis C virus
	HTV	Human immunodeficiency virus

HBV	Hepatitis B virus
LIGA	Lithographie, Galvanik Abformung

BRIEF DESCRIPTION OF THE DRAWINGS

5 Figure 1 is an illustration of the dependence of the electrical field penetration depth in the case of a planar structure with the electrodes geometry (different ratios of (electrode width)/(electrode interspacing)) and dimension, L.

10 Figure 2 is a schematic drawing of the active sensor test site area of an embodiment of a bioelectronic sensor according to the present invention. Numbering used in Figures 2-7 is as follows: (1) direction of evaporation or deposition of metal; (2) first bonding pad of one sensor; (3) second bonding pad of one sensor; (4) 'even' planes of electrode fingers; (5) 'odd' planes of electrode figures; (6) hills, blocking planes (4) from (5); (7) channels; (8) mask for separation of different sensors; (9) shaded arrays (shaded from metal deposition); (10) probes; (11) field lines of a sensor on which a voltage is applied; (12) to be detected molecules; (13) sacrificed electrodes
15 in the separation step; (14) width of all interdigitated electrodes together of one sensor; (15) left side of device with separate functions: electrodes; (16) right side of said device: area with probes.

20 Figure 3a is a schematic drawing, representing a base plate for making an array of 2x2 sensors (by way of example and not by way of limitation) according to an embodiment of the present invention; Figure 3b, 3c and 3d give a cross-sectional detail of one sensor according to the present invention. (The numbering used is as described for Figure 2)

 Figure 4a, 4b and 4c show schematically a metallization process of the sensor according to the present invention. (The numbering used is as described for Figure 2)

25 Figure 5a illustrates how a shadow mask is applied for achieving a final structure. Figure 5b shows the sensor array after etching through this mask. (The numbering used is as described for Figure 2)

 Figure 6 illustrates the working principle of one of the possible embodiment of the sensor according to the present invention. Figure 6a shows a sensor without 'recognized' molecules and

Figure 6b with 'recognized' molecules. (The numbering used is as described for Figure 2)

Figure 7a and 7b show a specific embodiment of the bioelectronic sensor of the present invention. (The numbering used is as described for Figure 2)

EXAMPLES AND DETAILED DESCRIPTION OF THE INVENTION

5 Preferred exemplary embodiments of the present invention will hereafter be described in conjunction with the appended drawings. It is to be understood that the examples given are only for the purpose of teaching of the invention, the spirit and scope of this patent application being limited only by the terms of the appended claims.

10 The sensor of the present invention comprises an insulating layer with metallic electrodes on the top. A submicron pattern is made in the insulating layer. The metal top layers are in a specific geometry thereby enhancing the detection sensitivity of the sensor. Said sensor can further comprise a base layer.

Figure 2 shows a detailed view of a preferred embodiment of an electronic sensor according to the present invention. This figure shows the active test site area of the sensor in a schematic drawing. This sensor or test site may be fabricated in a sequence of steps as detailed hereunder.

15 A substrate is to be provided. Said substrate, designating said base layer, can be a crystalline wafer (quartz, silicon, germanium), an amorphous material (glass wafer), a polymer (PMMA, PC, PEEK, PVE, PEI) or thick film substrate, such as Al_2O_3 . An insulating layer is formed on said substrate. The insulating layer can be a polymer layer such as polyimide or BCB. The dielectric or insulating layer can as well be Si_3N_4 being deposited by LPCVD or PECVD techniques. It can also be a layer of SiO_2 that is deposited or thermally grown on said silicon wafer. A specific geometry can then be patterned using known lithography techniques, e.g. photolithography, preferably UV lithography, even more preferably deep UV lithography, followed by a selective etching in the SiO_2 layer. Another way to produce such insulating structure with a specific geometry is using a moulding process. The reproduction is then done by injection moulding or any other way of making replicates. The mould can then be made with LIGA using X-ray or photolithography, preferably UV lithography, more preferably deep UV lithography, which allows to achieve very small dimensions. Plastics such as PMMA, PEEK, PVE and PEI can be used as

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a substrate. The use of these plastics for making microstructures is known in the art.

The moulds fabricated by means of the above-defined methods can be used again as a tool for further replication processes, e.g. as mould inserts for micromoulding or reaction injection moulding. Materials to be used for the replication processes are usually melted polymers and casting resins. After hardening in the metallic form, the mould materials have reached a sufficient strength and the separation of mould and mould insert can take place. For the realization of micromoulding and micro-reaction injection moulding the extremely low roughness of the walls of LIGA fabricated mould inserts is most important.

Materials which have been used for microreplication include low viscosity thermoplastic polymers like polymethyl methacrylate (PMMA), polyoxymethylene (POM), polyamide (PA), or polycarbonate, as well as reaction resins based on methacrylates, silicones and caprolactames. However, many more materials could be used. Except for filled moulding materials, almost any material suitable for macroscopic moulding can be used for micromoulding.

Ceramic microstructures can be fabricated by slurry casting, by using sol-gel processes or by means of electrophoretic and other processes. It is e.g. possible to fill the gaps of a LIGA fabricated polymer structure with a slurry of microcrystalline ceramic powder. After drying and firing, the polymer degrades, evaporates or is oxidized, which results in a ceramic microstructure ("method of the lost form"). The characteristic dimensions of the ceramic structures are smaller than the polymer form, due to shrinkage during the firing process. Mechanically very stable and temperature persistent materials, piezoelectric materials and ionic conductors can thus be microstructured by means of the LIGA process.

Figure 3 shows a plate with 2x2 sensors. The chemical composition of this plate can be an insulating on its own or the plate can be composed of a substrate (e.g. a silicon wafer) with an insulating layer (e.g. a SiO₂ layer) thereon. The topography of the plate shows pits (7) and hills (6). Figure 3b gives a detail of one sensor, Figure 3c and 3d show cross-sectional views. In a preferred embodiment, the pits (7) are channels (7) having dimensions of the same order of magnitude as the molecules to be detected. Thus the channels are preferably about 100 nm deep and about 100 nm wide, about 100 nm spaced. The spacing in one direction defines adjacent planes (4) (5). The dimensions of the channels can range between about 500 nm deep and about

500 nm wide down to about 10 nm deep and about 10 nm wide, preferably less than 250 nm deep and less than 250 nm wide. This width and deepness may vary independently. The spacing between two channels is of the same order of magnitude as the width and deepness of the channels. The channels are as long as the length of the active test sites area of the bioelectronic sensor. In the sequel, and for the purpose of explaining the invention, this length is assumed to be 0.5 mm. Lengths between 100 μm and 1 mm or smaller or larger are possible. The active area can be made in any geometry, for production purposes by preference a square. It can as well be rectangular. Also the channels can have any shape, e.g. trapezoidal, triangular, rectangular or cylindrical.

The hills (6) are elevations of a specific height. In this embodiment a height of 1 μm is assumed. The height of the hills can be anything above the width of the channels. Their purpose is to separate the (4) and (5) planes between the channels. The shape of the hills by preference is rectangular but does not necessarily have to be so. The hills are located at the end of the planes (4) (5) between the channels compulsory depassing over the edge of the channel. If at one side of the sensor, they are located at the 'even' planes (4), then they are located at the 'odd' planes at the other side (5) (Figure 2b). In this embodiment, the hills are about 200 nm long and about 200 nm wide.

Figure 4 illustrates the next step in the processing. A metal layer is deposited on the plate under an angle, by preference by means of e-beam evaporation. The direction of the deposition is shown by the big arrow (1). The directionality has to be such that some places (9) on the plate are shadowed and not covered by metal. The angle of metal deposition therefore has to be smaller than 90° as measured with respect to the surface of the plate. By preference the angle of deposition is smaller than 60° , 45° and even smaller than 30° , such as 20° , 10° , 5° or 1° . Said places (9) are at the bottom of the channels and at the sidewalls of the channels and of the hills along the deposition direction (1). The planes (4) (5) between the channels are isolated one from another because there is no metal at the bottom of the channels and at the sidewalls along the deposition direction (1). Nor are they shortcuted at the edges due to the hills (6) (see Figure 2 for a 3-D impression). Any metal that does not react with the sample solution can be used. Examples are Pt, Pd, Au or less noble metals like Ag or Al provided that chemical reactions at the electrodes are expelled. The thickness of the metal layer or metal coating can range inbetween about 2 nm, 50 nm, 100 nm, 200 nm or thicker, preferably the metal thickness is 20 nm. The

metal deposition can be achieved using thermal evaporation, sputtering, e-beam deposition or any other technique known for depositing metals such as an impinging flux of metals.

The different sensors in an array (in this example 2x2 sensors) are however still shortcircuited. Selective etching of the evaporated metal separates the different sensors. Figure 5a shows the application of a mask (8). This mask can be lithographically transferred to a resist pattern, or it can be a shadow mask. If the structure is etched like this, the structures under the masking layer remain and the non-covered area is etched. Figure 5b shows the result of this etching in separated sensors. These separated sensors can be a possible final structure. These separated sensors with probes attached thereon are also a possible final structure. Separated bonding pads (2) and (3) are achieved and thus an interdigitated electrode structure results.

The shaded area of the mask (8) in figure 5a determines the active array of the sensor and the positive (2) and negative bonding pads (3). The open area of the mask is etched away (cf. above) and separates the different sensors from each other. The alignment of the mask (8) is not critical. An alignment accuracy of 10 μm is sufficient for this embodiment. The up and down sides in figure 5a are defining the bonding pads (2) and (3) and their final dimension is not critical. The dimensions of the left and right sides on figure 5a are not critical neither. The mask (8) is namely 50 μm smaller than the width (14) of all the channels. The final active area is thus determined by mask (8). Some fingers (13) are sacrificed and etched away. This means that a misalignment of half this width of 50 μm (i.e. 25 μm) does not have any influence, because the active area is still fully covered with channels (7) and the resulting finger electrodes (4) and (5), being the metallized planes. This procedure prevents from needing structuring methods with a sub-micron resolution.

Other methods known in the art to separate the different sensors may also be used within the scope of the present invention.

Figure 6 shows one possible way of the working principle of a sensor of the present invention. Probes (10) may be immobilised in the insulating areas of the channels according to probe immobilization methods known in the art as such epoxy linkage, carbodiimide, reductive amination, cyanogen bromide, succinimide, carbodiimidazole, tresyl and tosyl chloride, divinyl chloride, maleimide, hydrazide, iso(thio)cynates and more preferred silanization with amino silanes, epoxysilanes, thiocyanato silanes, isocyanato silanes, succinic anhydride silanes, sulfhydryl silanes, caprolactam silanes and so on. However, in other measurement configurations and/or set-

ups, the probes can be selectively immobilised:

-only on metallic surfaces, for example by adsorption of sulfur containing moieties at a Au layer,

- or all over the active test site area: on the insulating and the conductive layers, for example by a sequential immobilisation process or by plasma polymerisation of an organic layer exhibiting reactive groups, like amino, sulfhydryl, aldehydes, carboxyl, hydroxyl and so on.

The probes in the context of the present invention may be, by way of example and not by way of limitation, enzymes (with affinity for specific substrates), oligonucleotides (with affinity for specific DNA and RNA fragments), antibodies (with affinity for specific antigens), antigens (with affinity for specific antibodies), or any other component of a analyte/coanalyte complex.

By applying an electrical signal, i.e. voltage or current, on the bonding pad (3) and bonding pad (2) an electric field arises, resulting in electric field lines (11). If the analyte to be detected (12) is in a sample solution it will bound to the specific probes (Figure 6b), resulting in a change in the electric field (11) in contrast with the situation depicted in Figure (6a). This change can be quantitated by measuring the impedance at the proper frequency and/or dc bias. By preference this electrical measurement is an impedance analysis, which can devolve in a measurement of resistance, capacitance, dielectric loss and/or reactance over a frequency range, including or not dc bias, or a combination of these techniques.

Due to the sub-micron dimensions of the channels and due to the shape of the electrodes (emerging from the deposition of metal under an angle), the electric fields (11) strongly penetrate in the region with the immobilised probes (11). An even stronger confinement of the electrical fields in the region of interest would be achieved in case when a second insulating layer is put on top of the (4) and (5) planes. In this way the electrical field lines probe more the interior of the channels where the bound analyte occupies most of the space.

When fabricating a sensor according to the present invention with the smaller dimensions (sub 100 nm) larger molecules that have to be detected might not enter the channels anymore due to steric hindrance. Figure 7 shows schematically how this problem can be overcome. A sensor is to be fabricated that can be split in two. The left side (15) of the sensor consists of an array of sensors with the interdigitated electrode structure, fabricated in the same way as discussed above.

The right hand side (16) has the mirror image of the sensor array and is covered with immobilized probes (10). The sample solution comprising the molecular structures and elements that are to be detected is put (incubated) on top of the right hand side (16). Certain molecules (12) will bind to the probes (10). After this recognition process, the sensor is closed by folding (Fig. 7b). The application of mechanical force brings the probes (10) and molecules (12) close enough to the interdigitated electrode structure, so that eventually a difference in impedance of the incubated versus a not incubated structure can be measured.

The present invention describes sensors which are suitable for real time measurements, i.e. the binding process during different incubation steps, with or without different condition changes, like for instance temperature.

The present invention also allows very flexible measurement set-ups such as analyte immobilisation on the surface of the sensing device and recognition of certain probes applied in the solution phase.

The described technological process and the high sensor miniaturisation also allow the construction of microdiagnostic devices.

Sensor arrays comprising different probes can be fabricated in the way just described, to result in microdiagnostic devices. Said integrated microdiagnostic devices are capable of simultaneous detection of a multitude of parameters, i.e. multiparameter testing. This is of particular importance for limited sample situations like in the case of neo-natals blood samples, for reliable diagnosis requirements like in the case of transplantation immunology, autoimmune diseases or blood-infections and ultimately for screening assays.

Such juxtaposed microdiagnostic arrays have the additional advantage that they can process parallelly and simultaneously several different samples.

CLAIMS

1. Sensor comprising :

- an insulating layer with a plurality of interspaced channels therein having essentially the same direction, said channels having a bottom and at least two opposite sidewalls along said direction ;
- a metal coating being applied on at least part of one of said two opposite sidewalls of essentially each channel and on at least part of the top of the insulating layer in between said channels thereby forming part of an impedimetric device comprising 2 electrodes.

2. Sensor according to claim 1 further comprising hills, with said hills:

- being located at the end(s) of the planes between said channels,
- having a height which is larger than the width of the channels, and,
- overlapping the plane between said channels and part of two adjacent channels.

3. A sensor according to claims 1 or 2 further comprising probes for binding to molecular structures present in a sample to be tested, said probes being applied to either the insulating part of the channels and/or to the surface of the electrodes.

4. A sensor according to any of claims 1 to 3 wherein said insulating layer is applied on a base layer substrate.

5. A sensor according to claim 4 wherein said substrate is a silicon wafer.

6. A sensor according to any of claims 1 or 5 wherein the dimensions of said channels are within a range of 10 nm to 500 nm.

7. A sensor according to claim 6 wherein said channels are 100 nm deep and 100 nm wide, said channels being interspaced by 100 nm.

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8. A sensor according to any of claims 1 to 7 wherein said insulating layer is a thermally grown SiO_2 .

9. A sensor according to any of claims 1 to 7 wherein said insulating layer is a polymer.

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10. A method of producing a sensor, said method comprising the steps of:

- forming a plurality of interspaced channels in a insulating layer, said channels having essentially the same direction, said channels having a bottom and at least two opposite side-walls along said direction and optionally hills as defined in claim 2;

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- depositing a metal layer on said insulating layer while aligning said insulating layer with respect to the metal deposition source such that the bottom of said channels and the sidewalls of said channels along the deposition direction are shadowed and not covered by metal to thereby form an impedance; and,

20

- optionally applying probes for binding to molecular structures present in a sample to be tested, said probes being applied to either the insulating part of the channels and/or to the surface of the electrodes.

11. A method according to claim 10 wherein the angle of metal deposition with respect to said insulating layer is smaller than 90° .

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12. A method according to claims 10 or 11 further comprising the step of applying said insulating layer on a base layer substrate.

13. A method according to any of claims 10 to 12 wherein said substrate is a silicon wafer and said insulating layer is thermally grown SiO_2 .

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14. A method according to any of claims 10 to 13 wherein the step of forming said channels is executed using microelectronics patterning techniques.

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15. A method according to claim 14 wherein the step of forming said channels is executed by a photolithographic process.

16. A method according to any of claims 10 to 15 wherein said insulating layer is a polymer.

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17. A method according to claim 16 wherein said polymer is structured by microstructure moulding.

18. A sensor obtainable by a method according to any of claims 10 to 17.

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19. A sensor apparatus for identifying molecular structures within a sample solution, comprising:

- a plurality of sensors according to any of claims 1 to 9 or 18;
- optionally an additional insulating layer applied above said sensor in order to confine the electrical field in said channel between the two separated parts of said metal layer;
- means for applying a voltage on the metal coatings; and

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- means for measuring the electrical properties or the impedance in between the electrodes of the sensors to determine which probes have bonded to (an) associated target molecule(s).

20. A sensor apparatus according to claim 19 further comprising connection means to said metal coatings, said connection means bordering the active area of said sensor and being oriented essentially perpendicular with respect to said direction and said voltage being applied on said connection means.

21. An array of sensors, said array being a geometric configuration of the sensors according to any of claims 1 to 9 or 18, the different sensors of the array being essentially parallel one to another along said direction.

22. Method for identifying molecular structures with in a sample solution comprising the steps of:

- applying said sample solution to a plurality of sensors, according to any of claims 1 to 9 or 18 or 21, each sensor having one or more probes applied therein to bond with an associated target molecular structure;
- applying an electronic signal to the sensor; and
- measuring the electrical properties of the sensor to determine which probes have bonded to (an) associated target molecular structure(s) such that a plurality of different targets can be detected.

23. A method according to claim 22 wherein said sensor have one or more types of oligonucleotide probes applied therein.

24. A method according to claim 22 wherein said sensor have one or more types of antibody

probes applied therein.

25. A method according to claim 22 wherein said sensor have one or more types of antigen probes applied therein.

5 26. A method according to claim 22 wheirein said sensor have one or more types of peptide probes applied therein.

27. A method according to any of claims 22 to 26 wherein said probes is (are) covalently or non-covalently attached to said sensor.

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28. A sensor according to any of claims 1 to 9 or 18 comprising one or more probe(s) applied to either the insulating part of the channels and/or to the surface of the electrodes, with said probe being as defined in any of claims 22 to 26.

15 29. A sensor apparatus according to any of claims 19 or 20 also comprising one or more types of probes applied to said sensors as defined in claim 28.

30. A sensor which is split in two parts and comprising:

- 20
- a first part comprising an array of sensors according to claim 21,
 - a second part comprising an array of containers to which probes may be attached, and,
 - with said first and said second parts being brought into contact in such a way that said array of containers corresponds to said array of sensors.

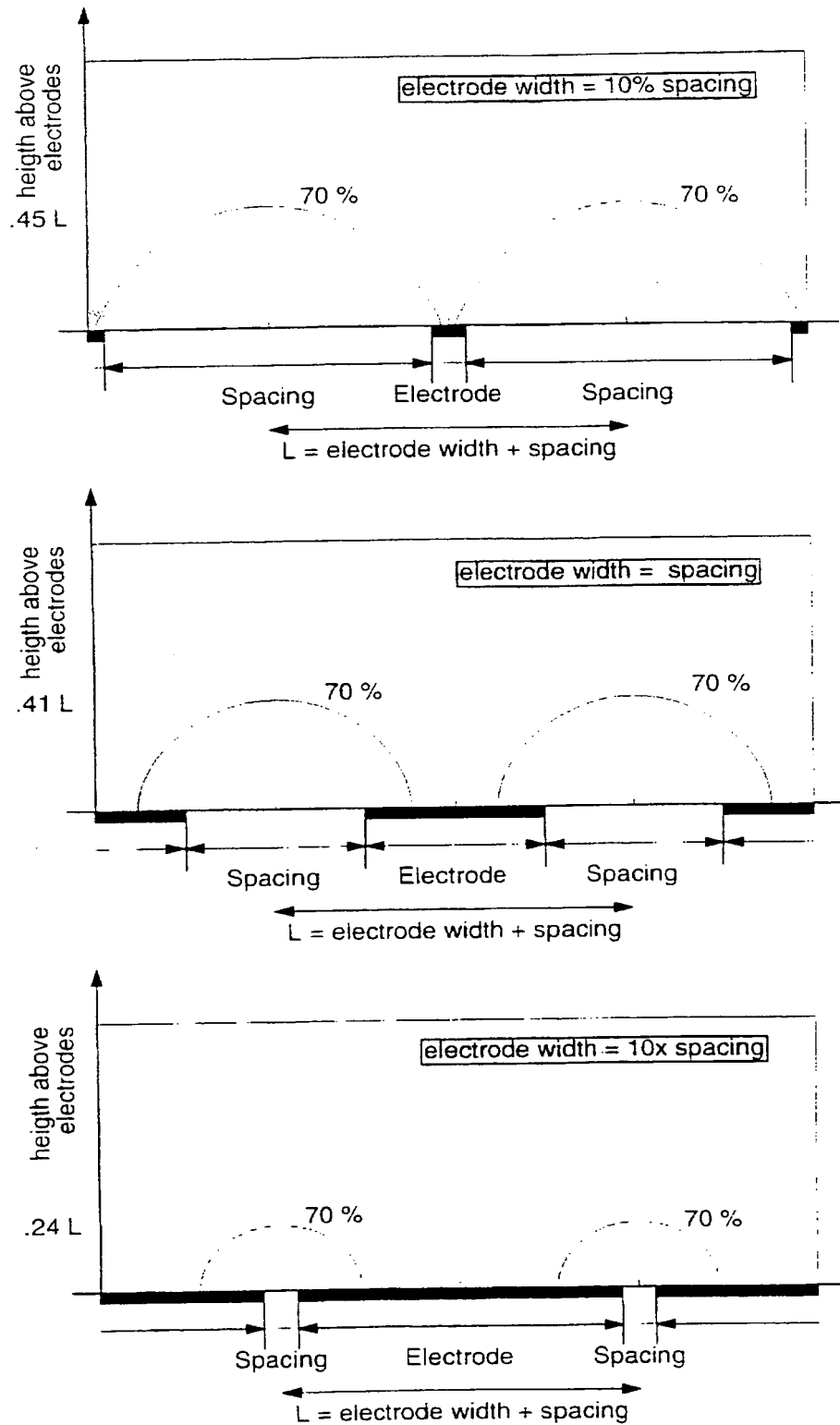


Figure 1

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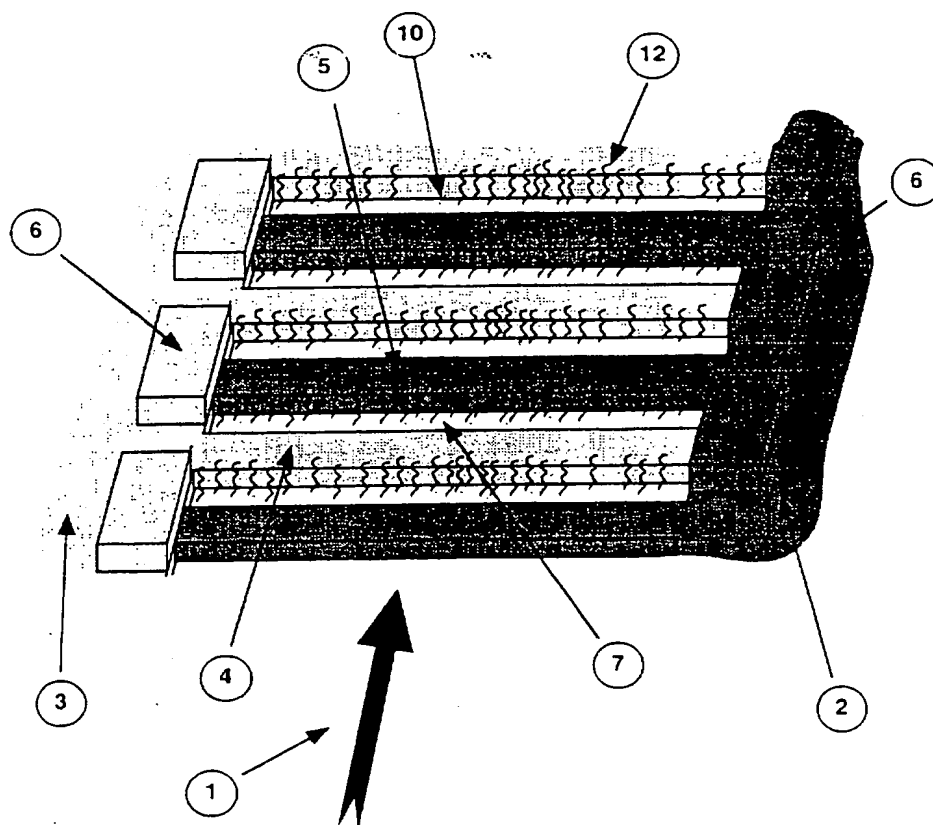


Figure 2

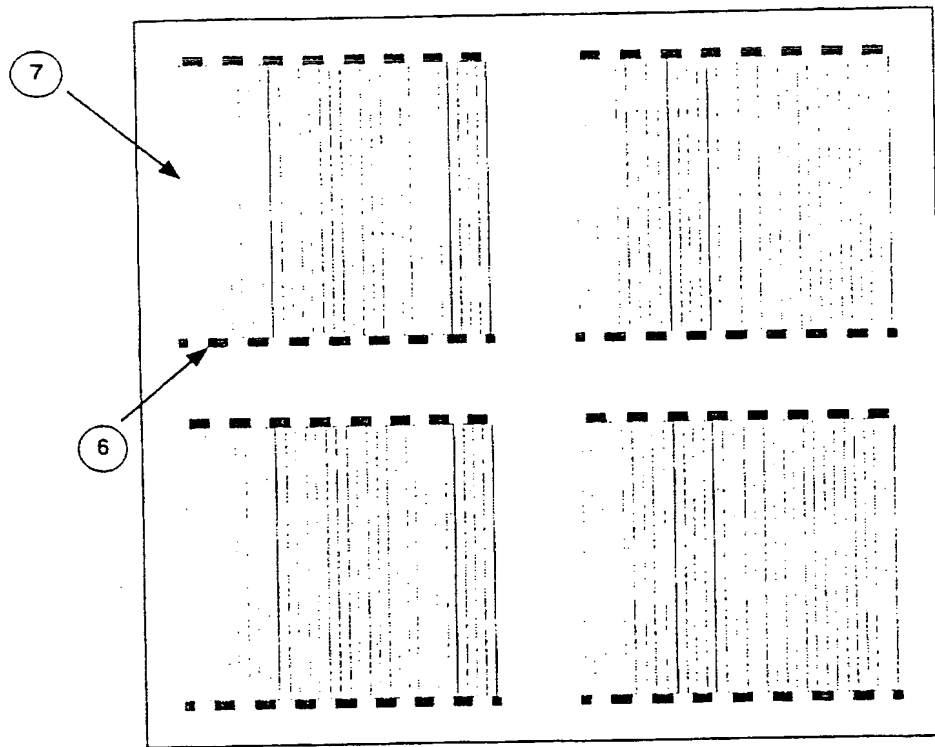


Figure 3a

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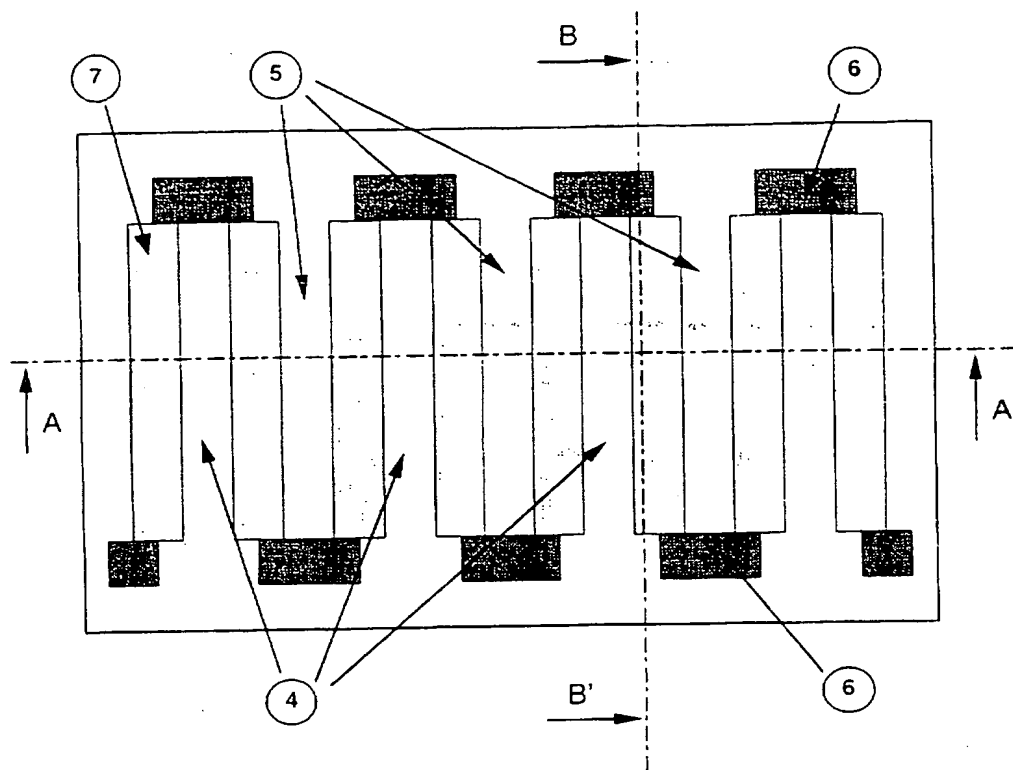


Figure 3b

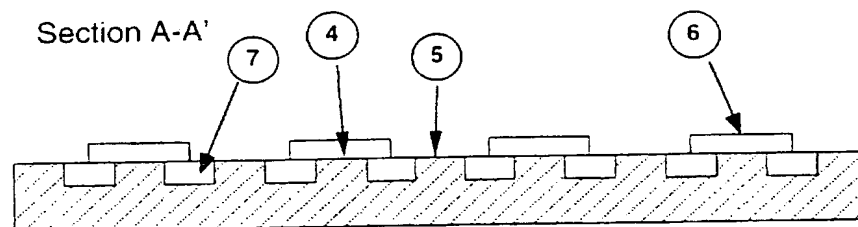


Figure 3c

Section B-B'

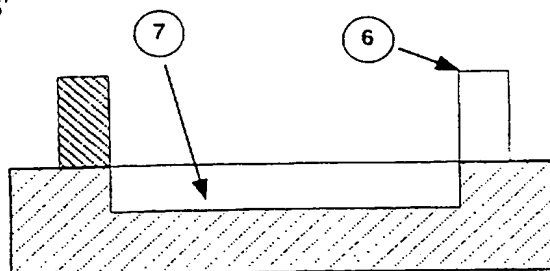


Figure 3d

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Section A-A'

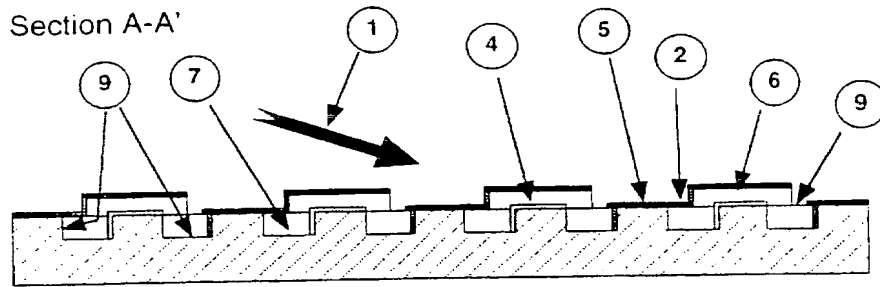


Figure 4a

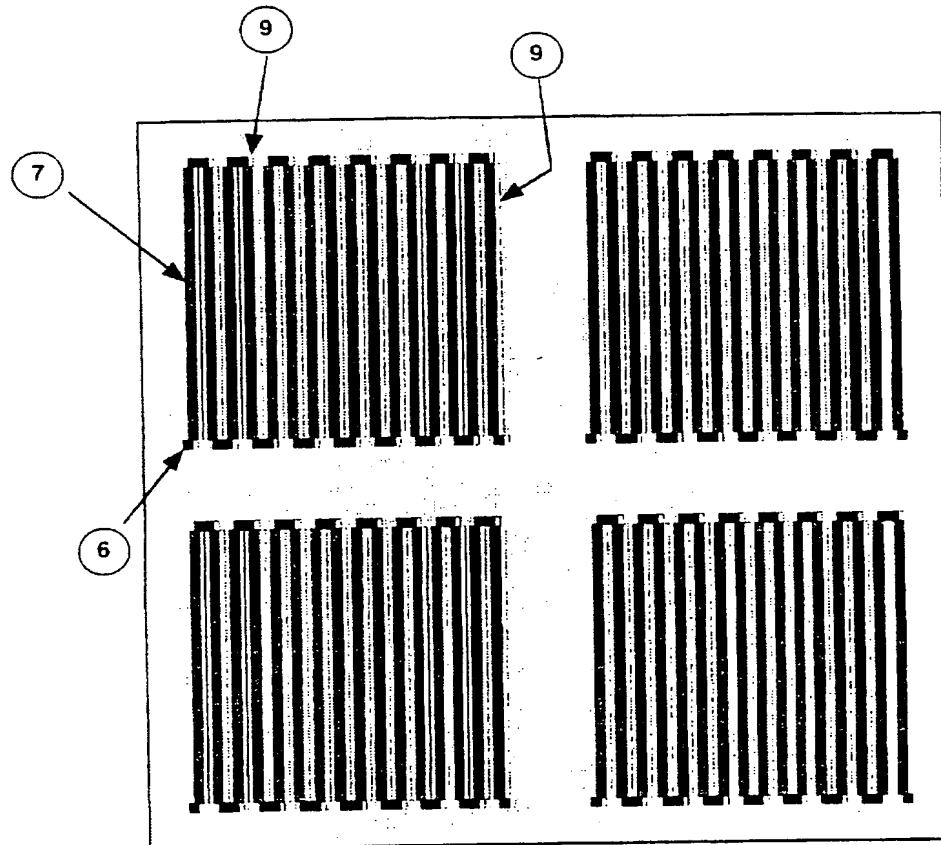


Figure 4b

Section B-B'

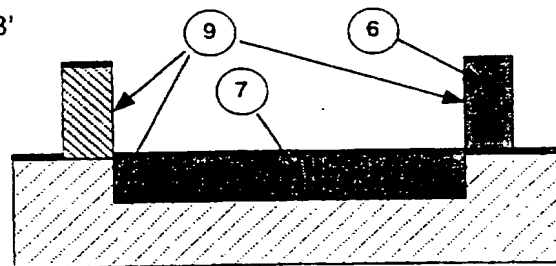


Figure 4c

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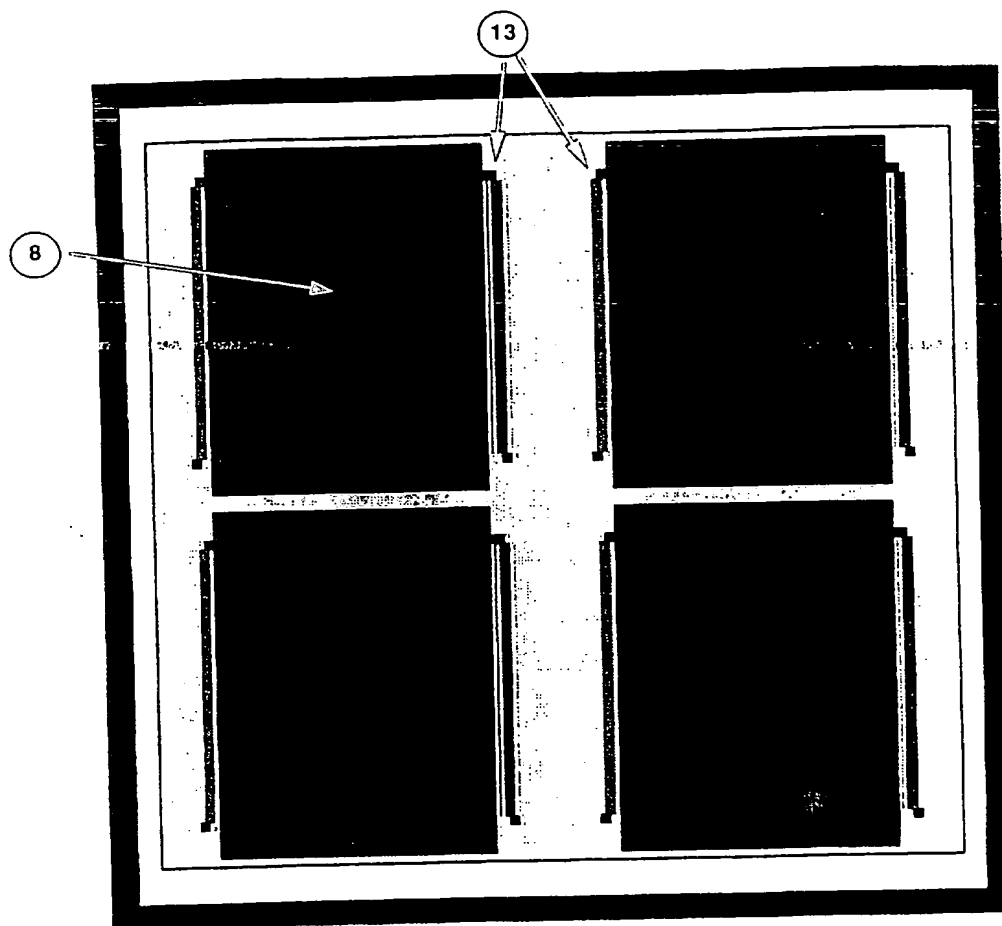


Figure 5a

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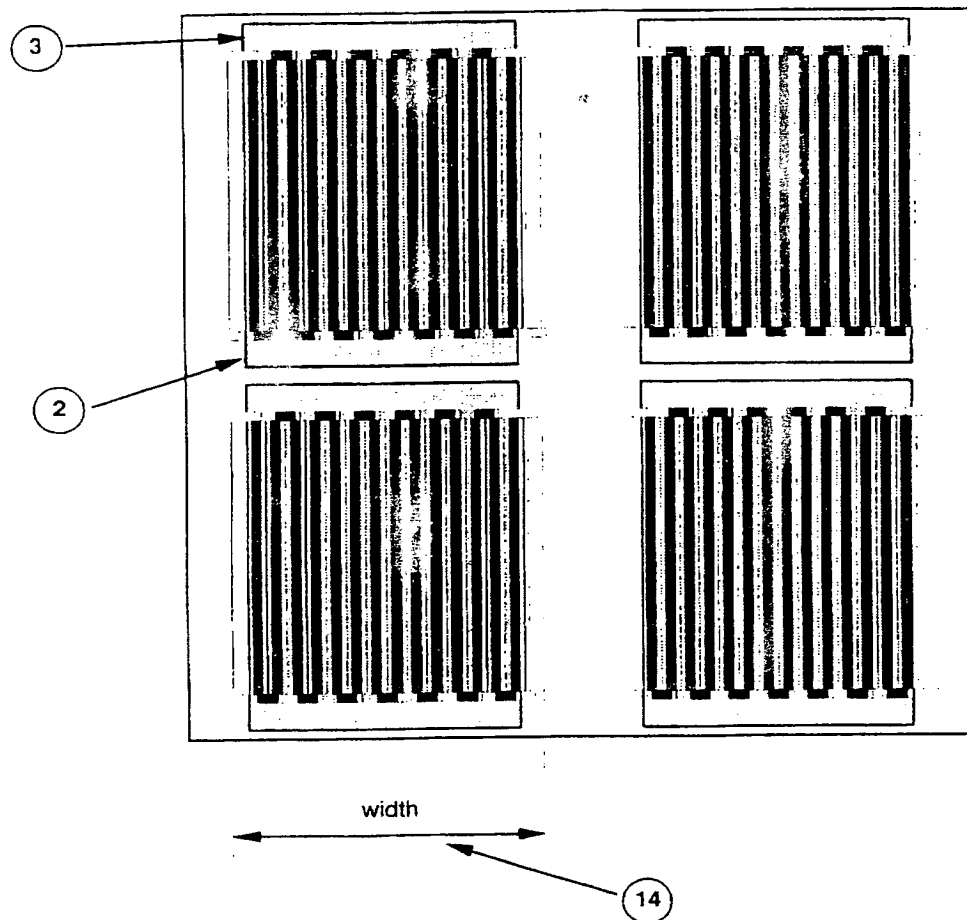


Figure 5b

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Section A-A'

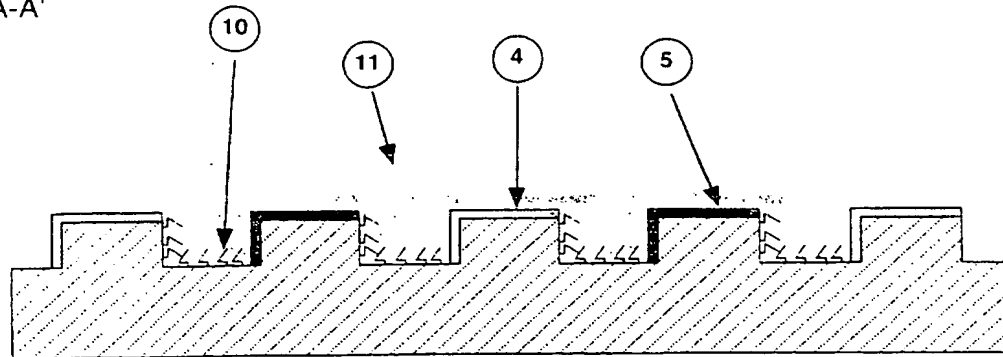


Figure 6a

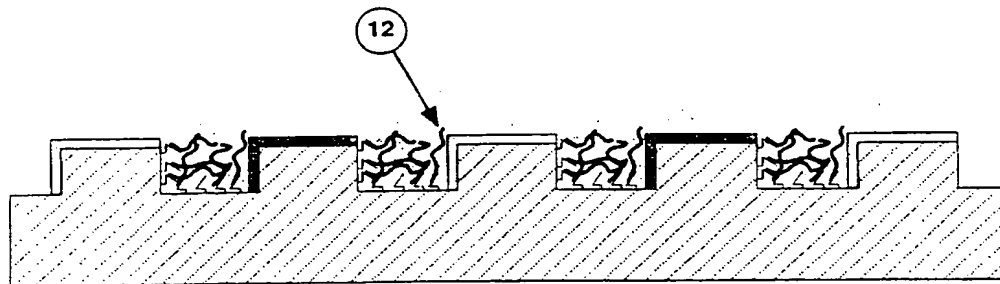


Figure 6b

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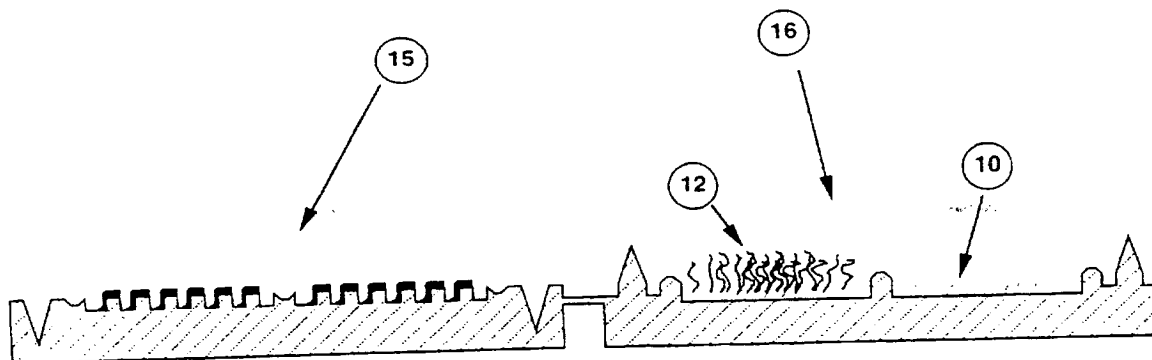


Figure 7a

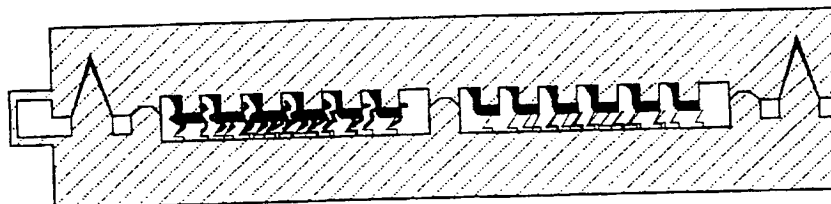


Figure 7b

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INTERNATIONAL SEARCH REPORT

International Application No.

PCT/EP 96/05290

A. CLASSIFICATION OF SUBJECT MATTER
 IPC 6 G01N27/22 G01N33/543 G01N27/02

According to International Patent Classification (IPC) or to both national classification and IPC:

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
 IPC 6 G01N

(Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched)

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

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Y	WO 93 22678 A (MASSACHUSETTS INST TECHNOLOGY ; BAYLOR COLLEGE OF MEDICINE (US); HO) 11 November 1993 see page 7, line 20 - page 24, line 20; figures 5,6	1,3-5,8,9
A		2,6,7,10-30
Y	GB 2 210 462 A (TOKYO SHIBAURA ELECTRIC CO) 7 June 1989 see abstract; figure 3	1,3-5,8,9
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☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex

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Date of the actual completion of the international search

19 March 1997

Date of mailing of the international search report

06.05.97

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Brison, O

INTERNATIONAL SEARCH REPORT

International Application No.

EP 96/05290

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
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Annex on patent family members

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